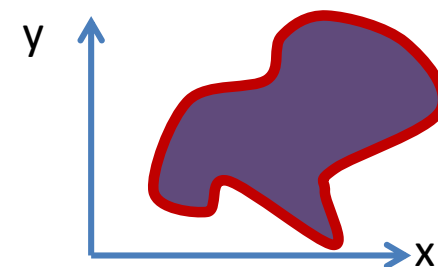


Stokes Theorem (16.8) and the Divergence Theorem (16.9)



Last Time: Green's theorem for a region in the plane

$$\int_C \vec{F} \cdot d\vec{r} = \int \int_A \left[\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right] dx dy$$

And we had a fancy way to write Green's theorem: Suppose $\vec{F} = (P(x, y), Q(x, y), 0)$

Then we have that $\nabla \times \vec{F} = (0, 0, \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y})$ (no z component)

So now we can write Green's theorem as

$$\int_C \vec{F} \cdot d\vec{r} = \int \int_A (\nabla \times \vec{F}) \cdot \vec{k} dA$$

So, we can think of Green's theorem as the following:

Collecting the tangential
component of a vector field
around a closed curve

=

The total flux of the vector field $\nabla \times \vec{F}$
through the surface enclosed by that
boundary

$$\int_C \vec{F} \cdot d\vec{r} = \int \int_A (\nabla \times \vec{F}) \cdot \vec{k} dA$$

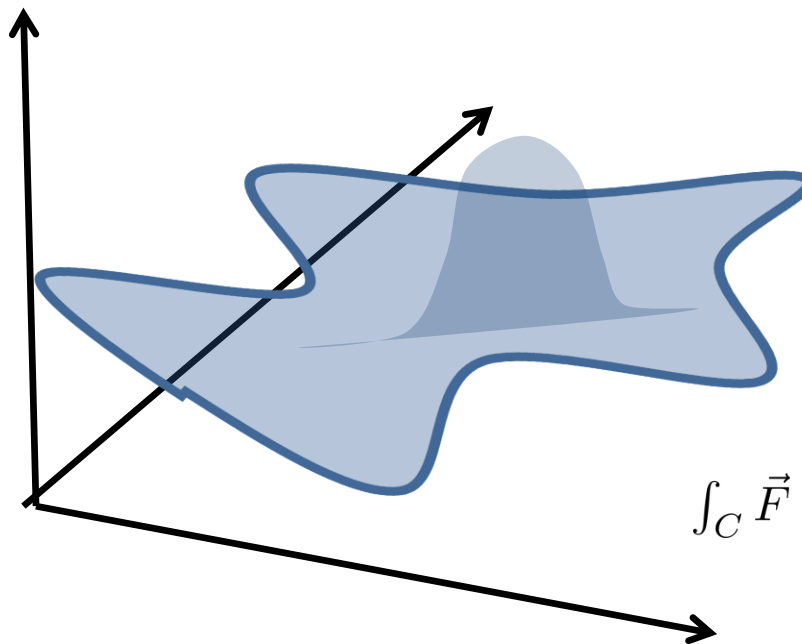
Collecting the tangential
component of a vector field
around a closed curve

=

The total flux of the curl of a vector field
through the surface enclosed by that
boundary

Stokes' Theorem

The same thing is true in 3D!!!



(this is supposed to be a
surface in 3D!).

$$\int_C \vec{F} \cdot d\vec{r} = \int \int_S (\nabla \times \vec{F}) \cdot d\vec{S}$$

$$\int_C \vec{F} \cdot d\vec{r} = \int \int_A (\nabla \times \vec{F}) \cdot \vec{k} dA$$

Collecting the tangential
component of a vector field
around a closed curve

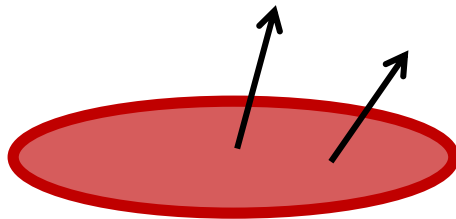
=

The total flux of the curl of the vector field
through the surface enclosed by that
boundary

Which immediately leads to a **remarkable statement**:

$$\vec{F} = \vec{F}(x, y, z)$$

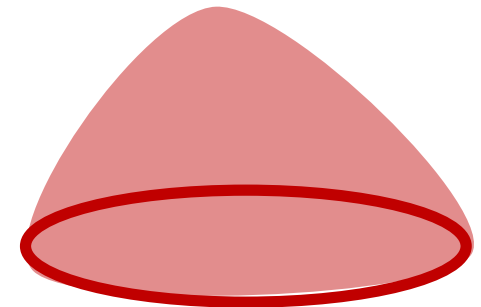
$$\vec{F} = \vec{F}(x, y, z)$$



=

Collecting the tangential
component of a vector field
around a closed curve

=



The total flux of the curl of a vector field
through the surface enclosed by that
boundary

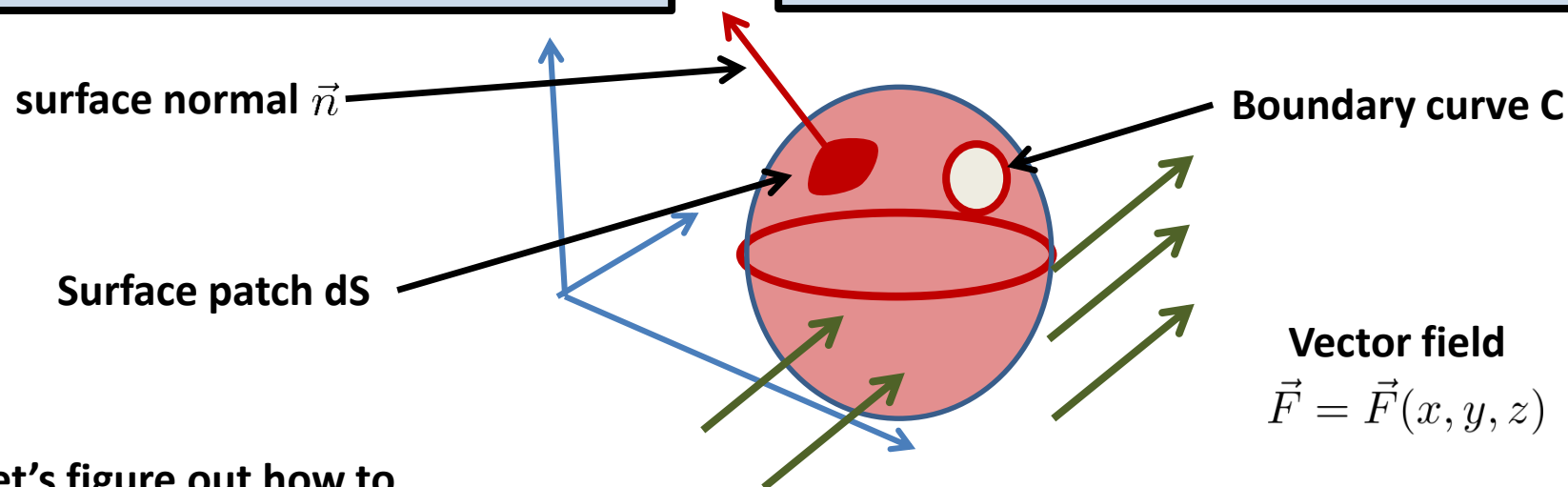
**These have to
be the same!!!**

The total flux of the curl of a vector field
through the surface enclosed by that
boundary

Collecting the tangential
component of a vector field
around a closed curve

=

The total flux of the curl of the vector field
through the surface enclosed by that
boundary



Let's figure out how to
write this theorem:

$$\int_C \vec{F} \cdot d\vec{r} = \int \int_S (\nabla \times \vec{F}) \cdot \vec{n} dS$$

Let's use it!

$$\int_C \vec{F} \cdot d\vec{r} = \int \int_A (\nabla \times \vec{F}) \cdot \vec{n} \, dS \quad \text{Example: Compute } \int \int_S \text{curl} \vec{F} \cdot d\vec{S} = \int \int_S \nabla \times \vec{F} \cdot d\vec{S}$$

where $\vec{F}(x, y, z) = xz\vec{i} + yz\vec{j} + xy\vec{k}$

and S is the part of the sphere $x^2 + y^2 + z^2 = 4$ inside the cylinder $x^2 + y^2 = 1$ and above the xy plane

Step 1: Make a drawing: the region is the “polar ice cap”

Step 2: Find the boundary curve

$$x^2 + y^2 + z^2 = 4 \text{ and } x^2 + y^2 = 1 \text{ so } 1 + z^2 = 4$$

$$\text{So the boundary curve is } x^2 + y^2 = 1 \text{ and } z = \sqrt{3}$$

Step 3: Parameterize boundary $\vec{r}(t) = \cos t \vec{i} + \sin t \vec{j} + \sqrt{3} \vec{k}$

Step 4: Find parameterized stretch factor $d\vec{r}(t) = \vec{r}'(t)dt = (-\sin t, \cos t, 0)dt$

Step 5: Evaluate the vector field in the parameterized coordinates

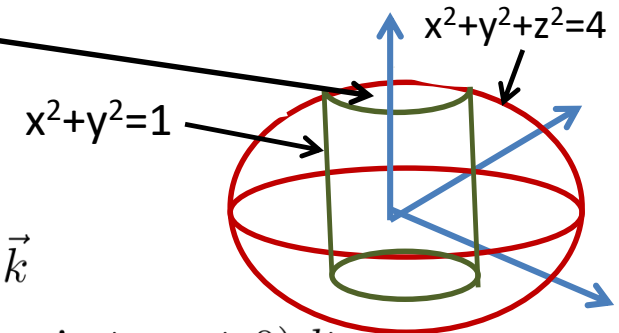
$$\vec{F}(\vec{r}(t)) = xz \vec{i} + yz \vec{j} + xy \vec{k} = \sqrt{3} \cos t \vec{i} + \sqrt{3} \sin t \vec{j} + \cos t \sin t \vec{k}$$

Step 6: Set up the integral

$$\int \int_A (\nabla \times \vec{F}) \cdot \vec{n} \, dS = \int_C \vec{F} \cdot d\vec{r} = \int_C \vec{F} \cdot \vec{r}' dt = \int_0^{2\pi} (-\sqrt{3} \cos t \sin t + \sqrt{3} \sin t \cos t) dt$$

Step 7: Do the integral!

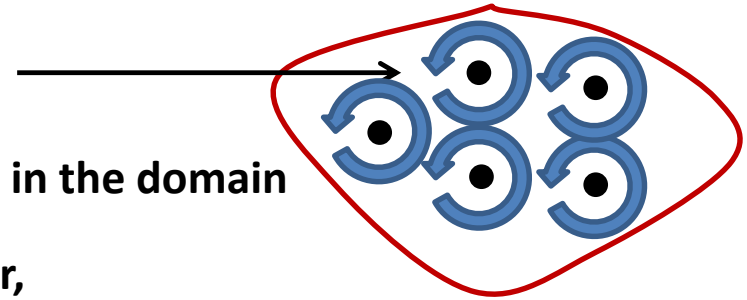
$$\int_0^{2\pi} (0) dt = 0$$



$$\int_C \vec{F} \cdot d\vec{r} = \int \int_A (\nabla \times \vec{F}) \cdot \vec{n} \, dS$$

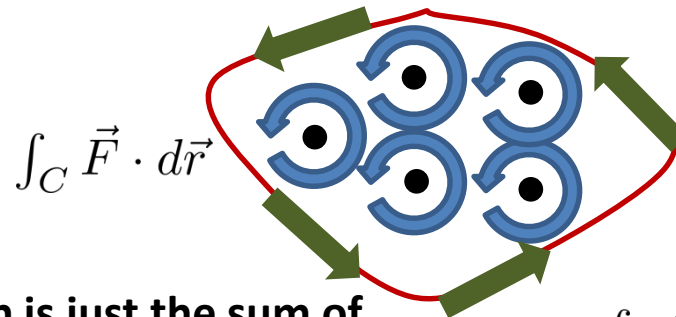
A partial proof is in the book—let me try and give you a “geometric feel” for why it’s true.

$(\nabla \times \vec{F})$ is the “twist” at a point in the domain



So $\int \int_A (\nabla \times \vec{F}) \cdot \vec{n} \, dS$ is adding up all the twists in the domain

All those twists together will fight with each other, causing the entire object to rotate



**CAUTION: THIS IS
NOT A PROOF!!!**

And the total rotation is just the sum of the vector field acting on the boundary

$$\int_C \vec{F} \cdot d\vec{r}$$

So: $\int_C \vec{F} \cdot d\vec{r} = \int \int_A (\nabla \times \vec{F}) \cdot \vec{n} \, dS$

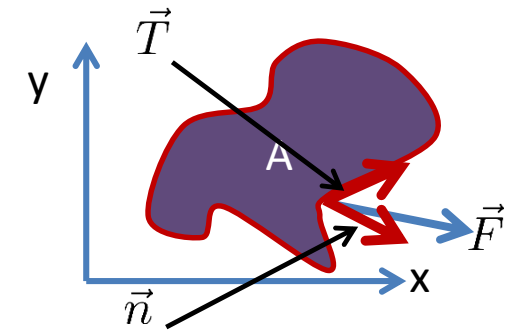
And there was nothing about that argument that required the surface or the curve to be flat!

What else can we do??? One more amazing theorem!

So now we've found that collecting the tangential component of the

vector field \vec{F} yields: $\int_C \vec{F} \cdot d\vec{r} = \int \int_A (\nabla \times \vec{F}) \cdot \vec{n} dS$

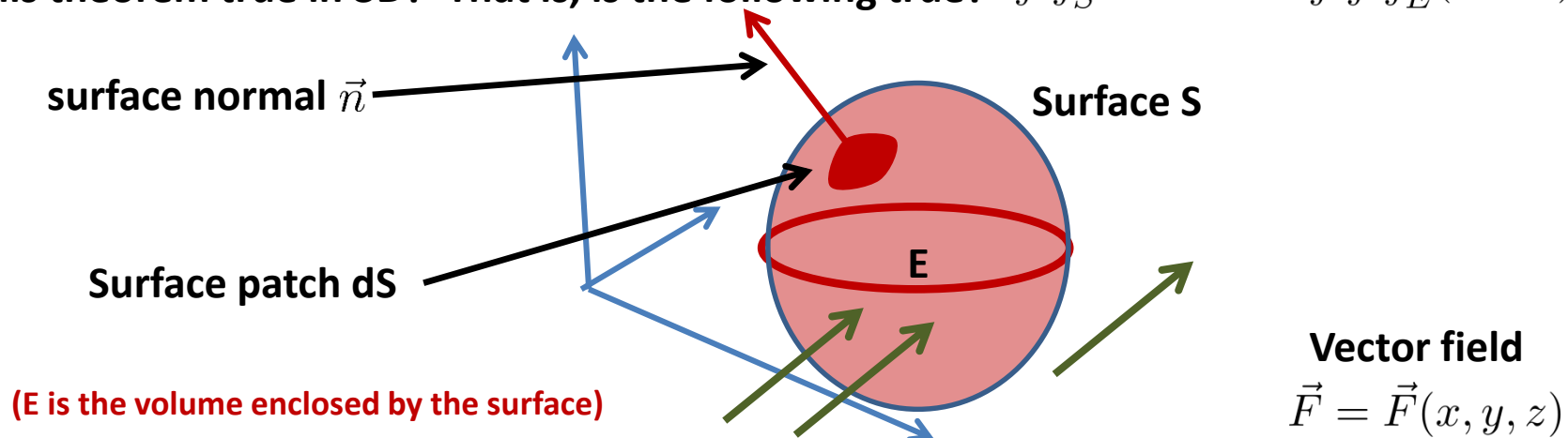
And neither the enclosed domain nor the bounding curve need to be flat



What happens if we try to collect the normal components of the vector field?

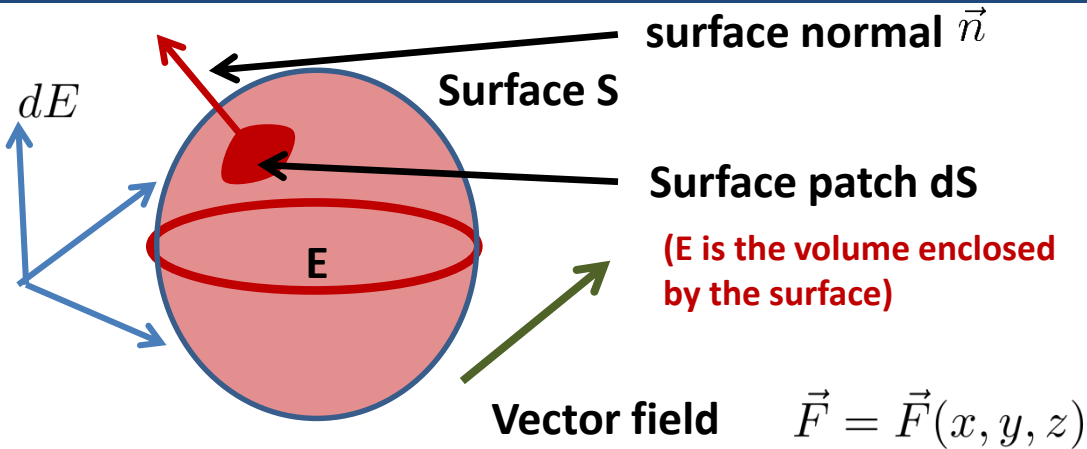
In 2D we have that $\int_C \vec{F} \cdot \vec{n} ds = \int \int_A (\nabla \cdot \vec{F}) dA$

Is this theorem true in 3D? That is, is the following true? $\int \int_S \vec{F} \cdot \vec{n} ds = \int \int \int_E (\nabla \cdot \vec{F}) dE$



Yes!!! $\int \int_S \vec{F} \cdot \vec{n} dS = \int \int \int_E (\nabla \cdot \vec{F}) dE$

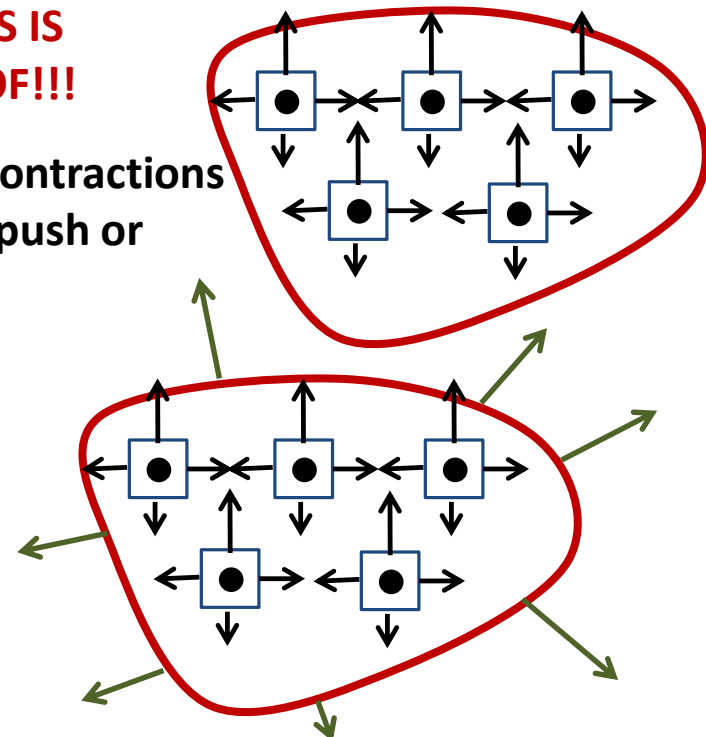
Again, let me give you a geometric feel as to why this is true....



$\nabla \cdot \vec{F}$ = Amount of expansion or contraction at a point

CAUTION: THIS IS *NOT* A PROOF!!!

is adding up all the expansions/contractions in the domain, and letting them push or retract against each other



So $\int \int \int_E (\nabla \cdot \vec{F}) dE$

and when these all push against each other, the net effect is felt as a normal push on the boundary...

And there was nothing about that argument that required the surface or the curve to be in 2D!

$$\int \int_S \vec{F} \cdot \vec{n} dS = \int \int \int_E (\nabla \cdot \vec{F}) dE$$

$$\vec{F} = \vec{F}(x, y, z)$$

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